

ACCUFORM METAL LTD.
TECHNICAL ROOF DECK INFORMATION
IMPERIAL UNITS

General – Load table contains factored strength and specified deflection uniformly distributed loads.

Steel - Conforms to ASTM A653 or ASTM A792, Grade 33 yield stress 33 ksi, tensile strength 45 ksi; Grade 40 yield stress 40 ksi, tensile strength 55.

Finishes - A25, G60, G90. For heavier metallic coatings, refer to ASTM A653 or ASTM A792.

Strength – The uniformly distributed factored strength load from the table must be equal to or greater than **[1.25(DL) + 1.50(LL)]**. Where **DL** is the specified dead load and **LL** is the specified live load.

Deflection (Serviceability) – The uniformly distributed specified deflection load from the table must be equal to or greater than the specified deflection live load. The effective moment of inertia for deflection determination was calculated at an assumed specified live load stress of **0.6F_y**.

EXAMPLE (Use of Table)

Given: AFRD 15-36 33 ksi

- ~ Deck thickness, $t = 0.048$ in.
- ~ Yield stress, $F_y = 33$ ksi
- ~ 2- span continuous, $L = 8.5$ ft each span
- ~ L/300 deflection limit (table is based on L/240)
- ~ Specified loads
 - 1) Dead load (DL)
 - a) Deck 3.0 psf
 - b) Superimposed 11.5 psf; DL = 14.5 psf
 - 2) Live load (LL) LL = 45.0 psf

Solution:

Strength “S”

- 1) Factored load $[1.25(14.5) + 1.50(45)] = \underline{85.6 \text{ psf}}$
- 2) Maximum factored load from load table is 89 psf
Since 89 > 85.6 ∴ OK
- 3) Check web crippling
 - a) End reaction $= 0.375(85.6)8.5 = \underline{273 \text{ lb/ft}}$
Assume bearing length $N = 1.5$ in.
From section property table,
 $P_e = P_{e1} + P_{e2} [N/t]^{1/2}$
 $= 731 + 183[1.5/0.048]^{1/2} = \underline{1754 \text{ lb/ft}}$
Since 1754 > 273 ∴ OK
 - b) Interior reaction $= 1.25(85.6)8.5 = \underline{910 \text{ lb/ft}}$
Assume bearing length $N = 3$ in.
From section property table,
 $P_i = P_{i1} + P_{i2} [N/t]^{1/2}$
 $= 1395 + 237[3/0.048]^{1/2} = \underline{3269 \text{ lb/ft}}$
Since 3269 > 910 ∴ OK

Deflection “D”

From table, $L/240 = \underline{75 \text{ psf}} > 45 \text{ psf}$ ∴ OK
 For L/300, multiply 75 by $240/300 = \underline{60.0 \text{ psf}}$
 Since 60.0 > 45 ∴ OK

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TECHNICAL ROOF DECK INFORMATION
METRIC UNITS

General – Load table contains factored strength and specified deflection uniformly distributed loads.

Steel - Conforms to ASTM A653M or ASTM A792M, Grade 230 yield stress 230 MPa, tensile strength 310 MPa; Grade 275 yield stress 275 MPa, tensile strength 380 MPa.

Finishes – ZF75, Z180, Z275 or AZM150. For heavier metallic coatings, refer to ASTM A653M or ASTM A792M.

Strength - The uniformly distributed factored strength load from the table must be equal to or greater than **[1.25(DL) + 1.50(LL)]**. Where **DL** is the specified dead load and **LL** is the specified live load.

Deflection (Serviceability) – The uniformly distributed specified deflection load from the table must be equal to or greater than the specified deflection live load. The effective moment of inertia for deflection determination was calculated at an assumed specified live load stress of **0.6F_y**.

EXAMPLE (Use of Table)

Given: AFRD 3-26 275 MPa

- ~ Deck thickness, $t = 0.914$ mm
- ~ Yield stress, $F_y = 275$ MPa
- ~ 3- span continuous, $L = 3.6$ m each span
- ~ L/180 deflection limit (table is based on L/240)
- ~ Specified loads
 - 1) Dead load (DL)
 - a) Deck 0.20 kPa
 - b) Superimposed 0.45 kPa; DL = 0.65 kPa
 - 2) Live load (LL) LL = 3.0 kPa

Solution:

Strength “S”

- 1) Factored load $[1.25(0.65) + 1.50(3.0)] = \underline{5.31 \text{ kPa}}$
- 2) Maximum factored load from load table is 5.82 kPa
Since 5.82 > 5.31 ∴ OK
- 3) Check web crippling
 - a) End reaction $= 0.40(5.31)3.6 = \underline{7.65 \text{ kN/m}}$
Assume bearing length $N = 75$ mm
From section property table,
 $P_e = P_{e1} + P_{e2} [N/t]^{1/2}$
 $= 6.35 + 1.59[75/0.914]^{1/2} = \underline{20.8 \text{ kN/m}}$
Since 20.8 > 7.65 ∴ OK
 - b) Interior reaction $= 1.10(5.31)3.6 = \underline{21.0 \text{ kN/m}}$
Assume bearing length $N = 100$ mm
From section property table,
 $P_i = P_{i1} + P_{i2} [N/t]^{1/2}$
 $= 13.0 + 2.21[100/0.914]^{1/2} = \underline{36.1 \text{ kN/m}}$
Since 36.1 > 21.0 ∴ OK

Deflection “D”

From table, $L/240 = \underline{3.53 \text{ kPa}} > 3.0 \text{ kPa}$ ∴ OK
 For L/180, multiply 3.53 by $240/180 = \underline{4.71 \text{ kPa}}$
 Since 4.71 > 3.0 ∴ OK